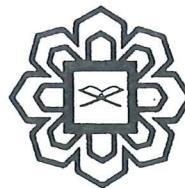


Name: _____

Matric No: _____ Section: _____



جامعة إسلامية دولية ماليزية

INTERNATIONAL ISLAMIC UNIVERSITY MALAYSIA

MID-TERM EXAMINATION
SEMESTER II, 2017/2018 SESSION
KULLIYYAH OF ENGINEERING

Programme : ENGINEERING Level of Study : UG 2

Time : 5:15 pm-7:15 pm Date : 05/04/2018

Duration : 2 Hours

Course Code : EECE 2313/ ECE 2133 Section(s) : 1, 2

Course Title : Electronic Circuits

This Question Paper consists of Five (5) Printed Pages (Including Cover and a blank page) with Three (3) Questions.

INSTRUCTION(S) TO CANDIDATES

DO NOT OPEN UNTIL YOU ARE ASKED TO DO SO

- Use only pen for writing answer.
- Do not use your own sheet.
- A total mark of this examination is 60.
- This examination is worth 30% of the total assessment.
- For drawing you may use pencil
- Answer ALL THREE(3) questions.
- Answer on the question paper.

Any form of cheating or attempt to cheat is a serious offence which may lead to dismissal.

	Question 1	Question 2	Question 3	Total Marks
Marks	20	20	20	60
Marks Obtained				

Q.1 [20 marks]

- (a) Consider the circuit as shown in Fig. 1(a), derive the expression (step by step) for the voltage transfer function $T(s) = v_o(s)/v_i(s)$. Find the corner frequency of the circuit if $R_s = 3 \text{ k}\Omega$, $R_p = 9 \text{ k}\Omega$ and $C_{p1} = 8 \text{ nF}$ and $C_{p2} = 8 \text{ nF}$. (6+2 marks)

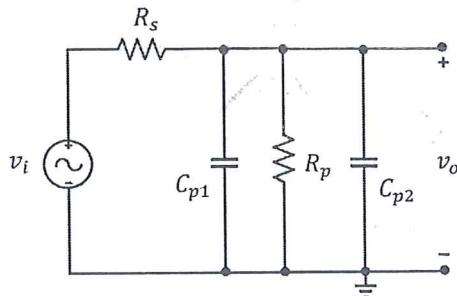


Fig. 1(a)

$$C_p = C_{p1} + C_{p2}$$

$$Z_p = R_p \parallel \left(\frac{1}{sC_p} \right)$$

$$= \frac{R_p \times \frac{1}{sC_p}}{R_p + \frac{1}{sC_p}} = \frac{R_p}{1 + sR_p C_p}$$

$$Z_{p+R_s} = \frac{R_p}{1 + sR_p C_p} + R_s = \frac{(R_p + R_s) + sC_p R_p R_s}{1 + sR_p C_p}$$

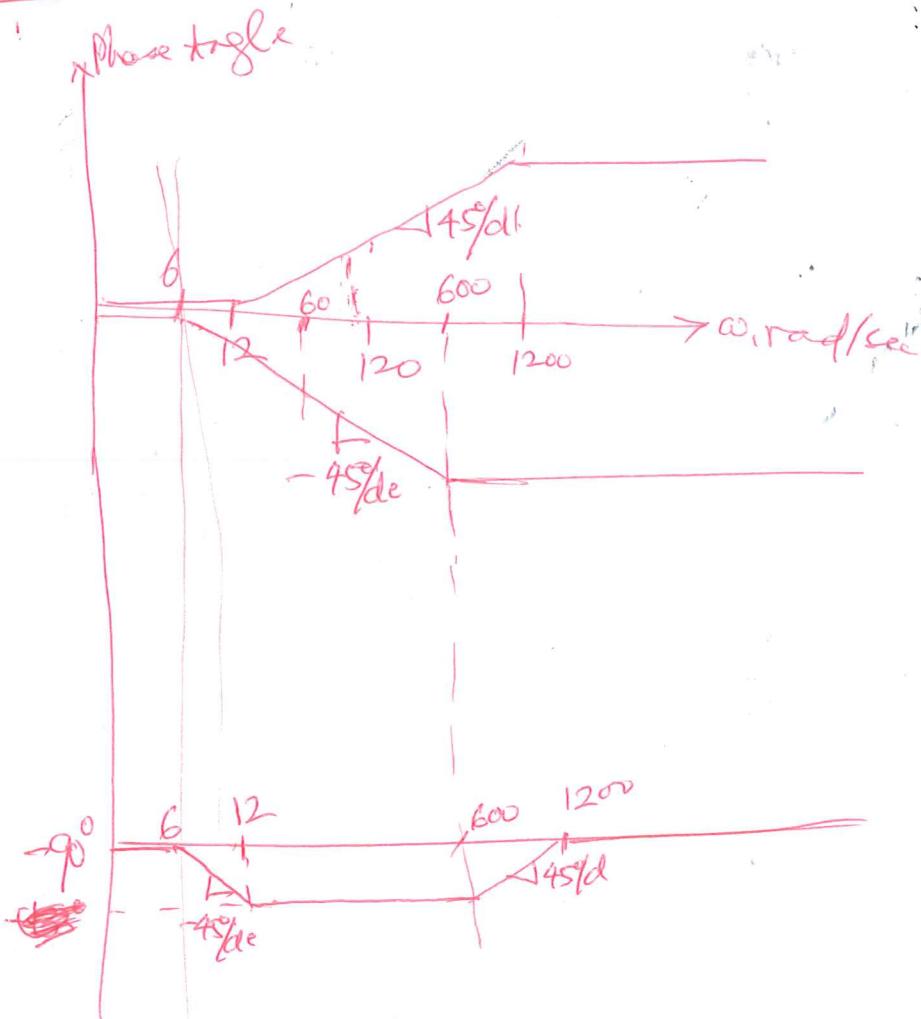
$$T(s) = \frac{V_o(s)}{V_i(s)} = \frac{Z_p}{Z_{p+R_s}} = \frac{\frac{R_p}{1 + sR_p C_p}}{\frac{(R_p + R_s) + sC_p R_p R_s}{1 + sR_p C_p}} = \frac{\frac{R_p}{(1 + sR_p C_p)^2}}{(R_p + R_s) + sC_p R_p R_s} = \frac{\frac{R_p}{R_p + R_s + sC_p R_p R_s}}{1 + sC_p R_p}$$

$$= \frac{R_p}{R_p + R_s} \cdot \frac{1}{1 + s \frac{R_p R_s}{R_p + R_s} C_p} = \frac{R_p}{R_p + R_s} \cdot \frac{1}{1 + sC_p R_s}$$

$$\omega_c = R_p \parallel R_s \times C_p = \frac{(3)(9)}{2.5} \times \frac{(8+8)\text{nF}}{16\text{nF}} = 3.6 \times 10^5 \text{ rad/sec} = 36 \text{ kHz}$$

$$\therefore f_c = \frac{1}{2\pi\omega_c} = 4.429 \text{ kHz} \quad \leftarrow$$

Phase



$$\begin{aligned}\theta &= -90^\circ + \tan^{-1} \frac{120}{120} - \tan^{-1} \frac{120}{60} \\ &= -90^\circ + 39.80^\circ - 59.036^\circ = -109.23^\circ\end{aligned}$$

(b) Draw the Bode plot (magnitude and phase) of the following transfer function.

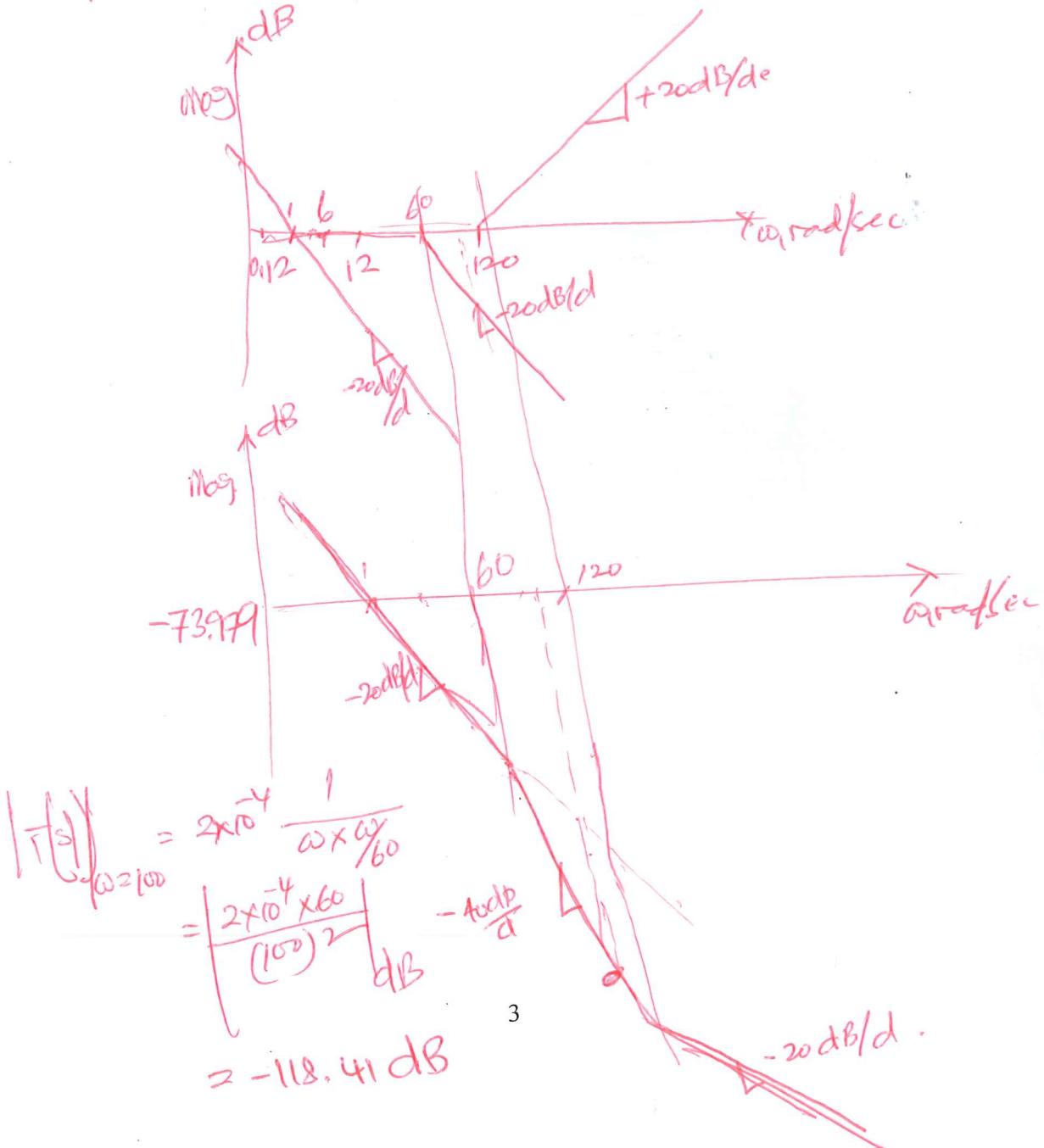
(8 marks)

$$T(s) = \frac{10^{-4}(s + 120)}{s(s + 60)}$$

(c) Determine the magnitude and phase at $s = 100$ rad/sec, using the solution from the graph of the question Q1.(b). (4 marks)

$$T(s) = \frac{10^{-4} \times 120 \left(1 + \frac{s}{120}\right)}{s \times 60 \left[1 + \frac{s}{60}\right]} = 2 \times 10^{-4} \times \frac{1 + \frac{s}{120}}{s \left(1 + \frac{s}{60}\right)}$$

$$T_1|_{ds} = 20 \log_{10} (2 \times 10^{-4}) = -73.979 \text{ dB}$$



Q.2 [20 marks]

A common source amplifier is shown in Fig. 2, with the following circuit component values $R_{Si} = 10k\Omega$, $R_G = 40k\Omega$, $R_S = 5k\Omega$, $R_D = 10k\Omega$, $R_L = 6 k\Omega$, $C_C = 3.2nF$ and $C_L = 1nF$. The MOSFET has a small - signal parameters, $g_m = 40 \text{ mA/V}$ and $r_o = \infty$.

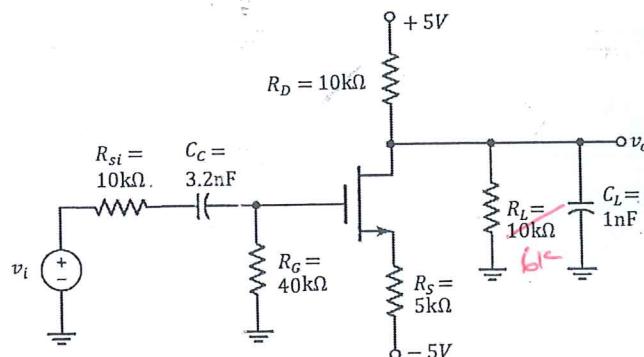


Fig. 2

- (i) Draw the small signal equivalent circuit diagram of the circuit. (3 marks)

(ii) Evaluate the midband voltage gain, $A_v = \frac{v_o}{v_i}$ of the amplifier in dB scale. (7 marks)

(iii) Determine the lower corner frequency, f_L (3 dB frequency) due to C_C . (4 marks)

(iv) Determine the higher corner frequency f_H . (4 marks)

(v) What is the bandwidth of the amplifier? (2 marks)

V_L
 $R_B = 40\text{ k}\Omega$
 $R_S = 5\text{ k}\Omega$
 $R_L = 3.75\text{ k}\Omega$
 C_E
 C_L
 $I_{in F}$
 V_O

$R_i = \infty$

$R'_L = R_L \parallel R_L = 3.75\text{ k}\Omega$

Q1
 $\Sigma_L = (R_S + R_Q) C_L$
 $= (10 + 140) \times 3.2\text{ nF}$
 $= 160\text{ }\mu\text{s}$

$R_O = \infty$
 $\Sigma_H = R_L \parallel C_L$
 $= 3.75\text{ }\mu\text{s}$

$f_L = \frac{1}{2\pi\Sigma_L} = 994.7\text{ Hz}$

$f_H = \frac{1}{2\pi\Sigma_H} = 42.44\text{ kHz}$

$BW = f_H - f_L = 41044.5\text{ kHz}$

$$AV_A = -\frac{g_m V_{GS} \alpha' R_L}{(V_{GS} + g_m V_{GS} R_S)} = \frac{V_o}{V_g}$$

$$= -\frac{-g_m R_L}{(1 + g_m R_S)} = -\frac{-40 \times 3.75K}{1 + 40 \times 15K}$$

$$= -0.746$$

$$Av = AV_A \times \frac{R_L}{R_S + R_Q}$$

$$= AV_A \cdot -0.746 \times \frac{40}{10 + 50} = -0.597$$

$$Av|_{dB} = 20 \log 0.597 = -4.48 \text{ dB}$$

Q.3 [20 marks]

- (a) Draw the simplified high-frequency model of a bipolar junction transistor (BJT) and mention the name of each parameter. (2 marks)
- (b) Draw the simplified high-frequency small-signal short-circuit ($R_C = 0$) equivalent diagram of the circuit as shown in Fig. 3(b), and determine the cutoff frequency f_T (step by step) for the transistor. (14 marks)
- (c) Assume that a BJT has the parameters, $r_\pi = 1.5\text{k}\Omega$, $g_m = \frac{20\text{mA}}{\text{V}}$, $C_\pi = 20\text{pF}$ and $C_\mu = 12\text{pF}$, determine the f_β and f_T of the transistor. (4 marks)

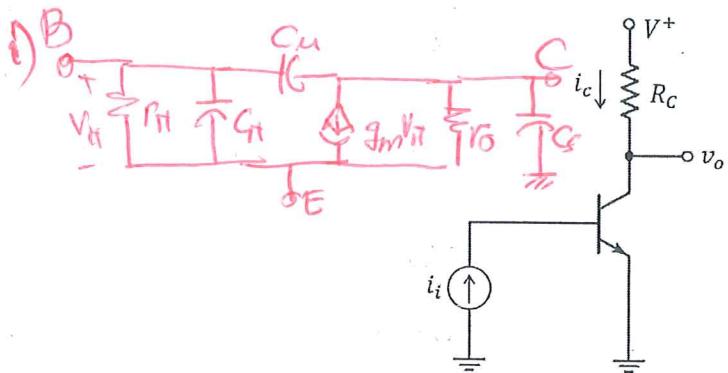


Fig. 3(b)

$$\begin{aligned}
 & \text{(i)} \quad \text{Fig. 3(b) equivalent circuit:} \\
 & \quad \text{Base current } I_B = \frac{V_B}{r_\pi} + sC_\pi V_{BE} + sC_\mu V_B = \frac{V_B}{r_\pi} \left[1 + s r_\pi (C_\pi + C_\mu) \right] \\
 & \quad \text{Collector current } I_C = \frac{V_B}{r_\pi} + sC_\pi V_{BE} + sC_\mu V_B = \frac{V_B}{r_\pi} \left[1 + s r_\pi (C_\pi + C_\mu) \right] \\
 & \quad \text{Emitter current } I_E = I_B + I_C = \frac{(g_m - sC_\mu)V_B}{r_\pi \left[1 + s r_\pi (C_\pi + C_\mu) \right]} = \frac{g_m r_\pi - sC_\mu r_\pi}{1 + s r_\pi (C_\pi + C_\mu)} \\
 & \quad \therefore A_{FE} = \frac{I_C}{I_E} = \frac{g_m r_\pi}{1 + s r_\pi (C_\pi + C_\mu)} = \frac{\beta}{1 + s r_\pi (C_\pi + C_\mu)} \\
 & \quad \text{At } f_T, \quad \frac{g_m r_\pi}{1 + s r_\pi (C_\pi + C_\mu) r_\pi} = \frac{\beta}{1 + s r_\pi (C_\pi + C_\mu)} \\
 & \quad \therefore \frac{g_m r_\pi}{1 + s r_\pi (C_\pi + C_\mu) r_\pi} \approx \frac{\beta}{1 + s r_\pi (C_\pi + C_\mu)} \quad [\because g_m r_\pi \gg \omega C_\mu r_\pi \text{ within freq of interest}] \\
 & \quad |A_{FE}| = 1 = \left| \frac{\beta}{1 + s r_\pi (C_\pi + C_\mu)} \right| \\
 & \quad = \frac{\beta}{\sqrt{1 + \left(\frac{\omega r_\pi (C_\pi + C_\mu)}{\beta} \right)^2}} \approx \frac{\beta}{\omega r_\pi (C_\pi + C_\mu)}
 \end{aligned}$$

$$\therefore N_T = \frac{\beta}{r_\pi (C_\pi + C_\mu)} \Rightarrow f_T = \frac{\beta}{2\pi r_\pi (C_\pi + C_\mu)} = \beta f_\beta =$$

$$\begin{aligned}\beta_2 g_m R_L \\ = 20 \times 15 \\ = 30\end{aligned}$$

$$f_T = \frac{\beta}{2\pi R_L (C_{in} + C_T)}$$

$$= \frac{30}{2\pi \times 1.5 \times 32 \mu} = 99.4718 \text{ MHz} \leftarrow$$

$$f_T = \beta f_B \Rightarrow f_B = \frac{f_T}{\beta} = 3.3157 \text{ MHz} \leftarrow$$