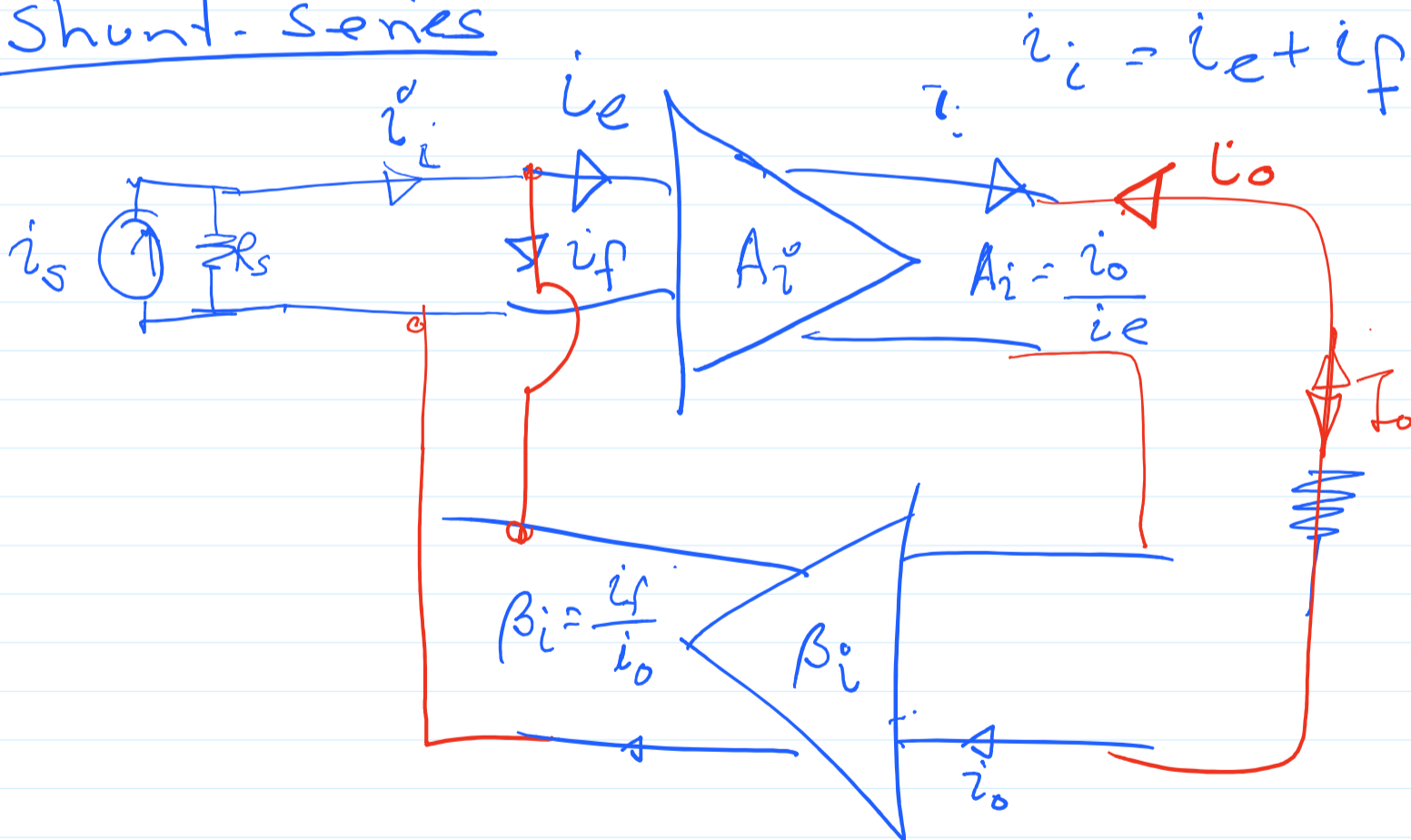


write down types of feedback amplifier topology and their types of amplification (type of amplifier)

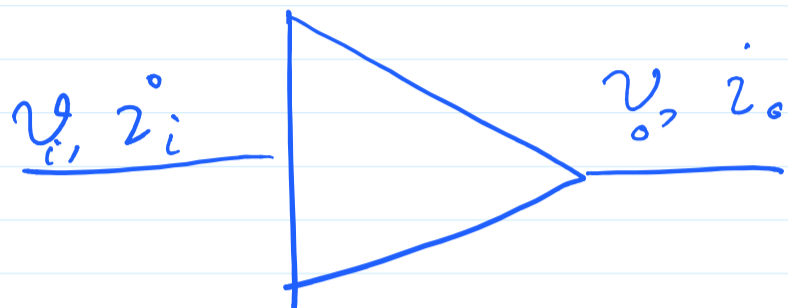
| | Topology | | Amplifier type |
|---|------------|--------------|---------------------------------|
| 1 | Series (v) | - Shunt (v) | Voltage Amplifier (Av) |
| 2 | Shunt (i) | - Series (i) | Current Amplifier (Ai) |
| 3 | Series (v) | Series (i) | Transconductance Amplifier (Ag) |
| 4 | Shunt (i) | Shunt (v) | Transresistance Amplifier (Az) |

Shunt-Series

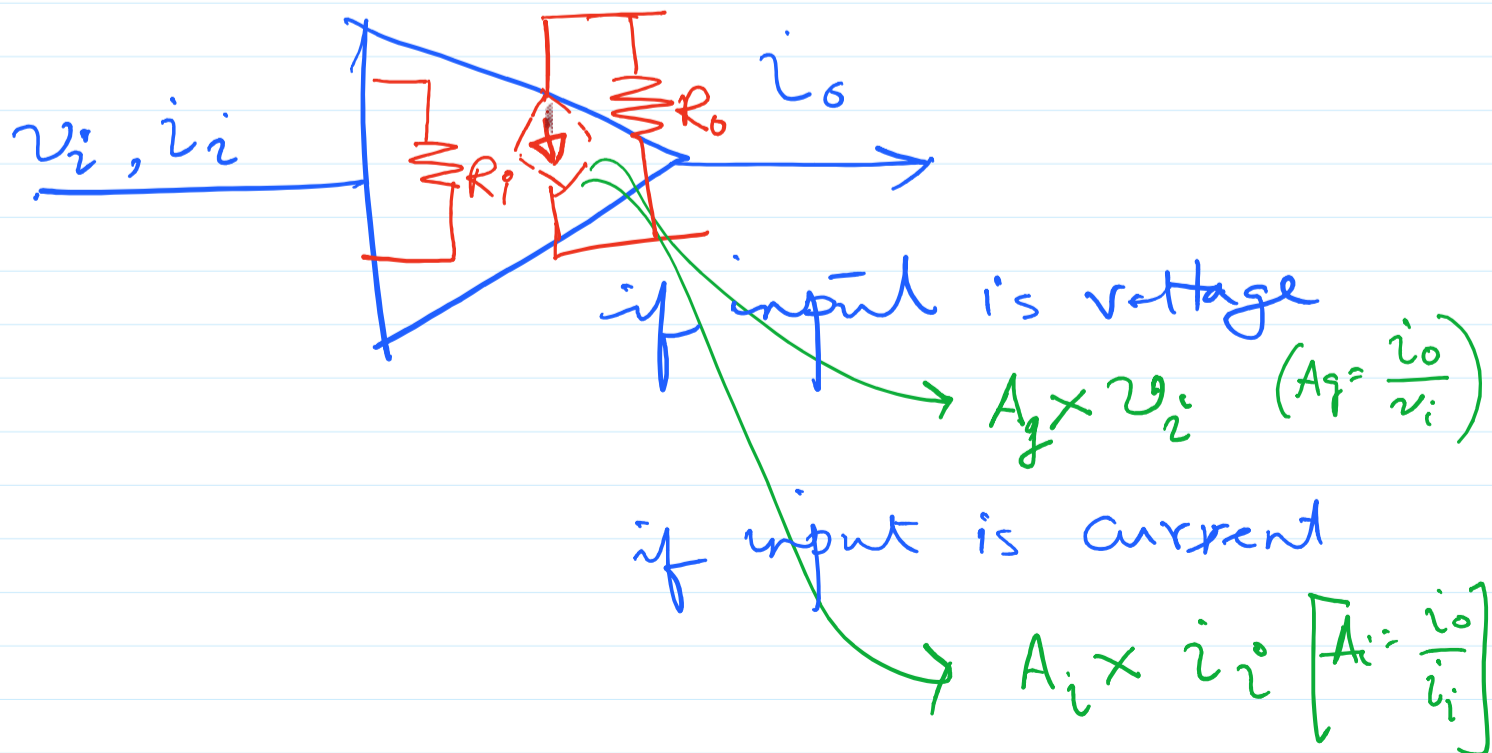
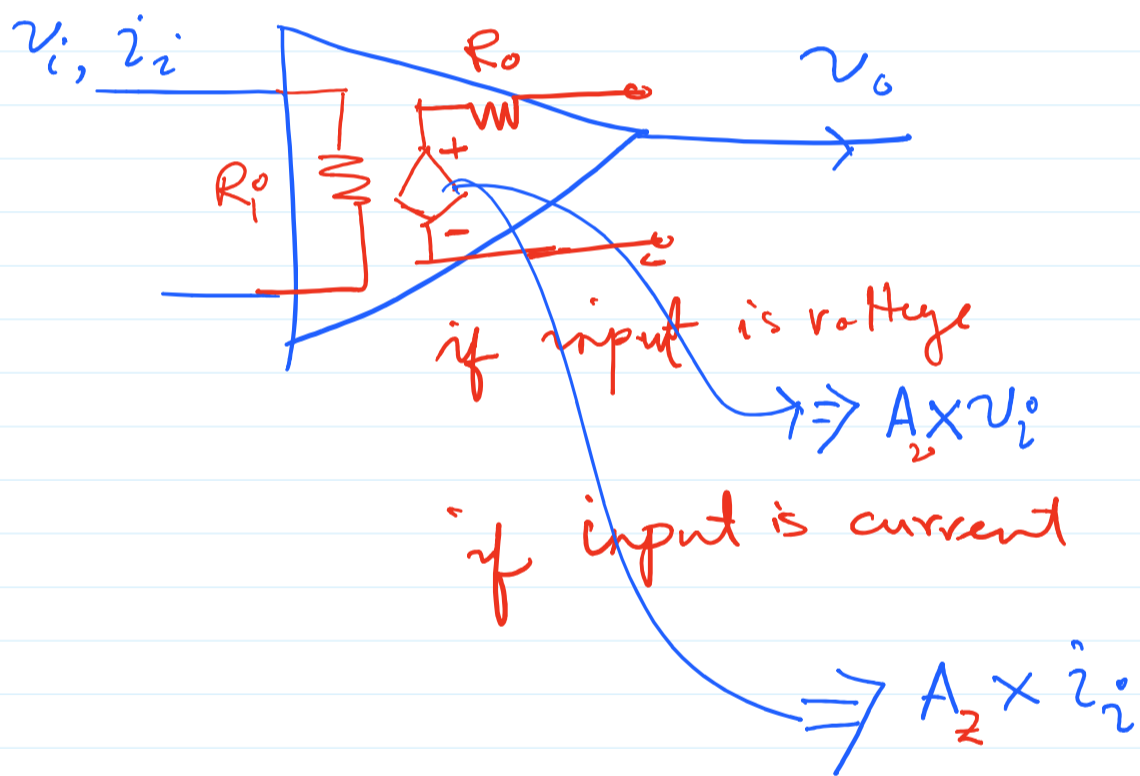


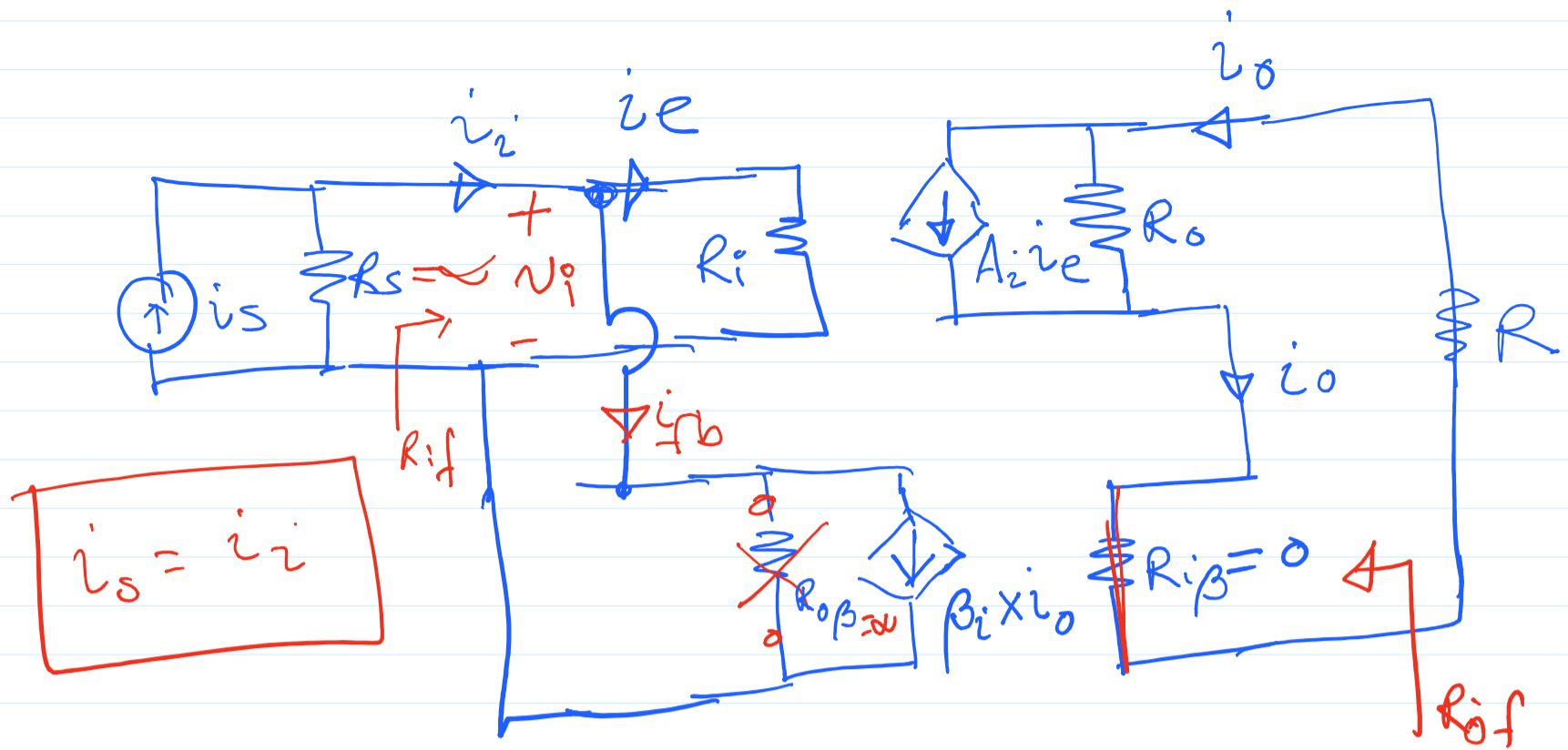
- i) Block diagram
- (ii) Small signal equivalent CKT.
- (iii) Ideal small signal equ. CKT

- (iv) a) Closed loop gain A_{if}
 b) Input resistance R_{if}
 c) Output resistance R_{of}



Output is voltage.





$A_{if} \rightarrow$ output (i_o)
 $R_{if} \rightarrow$ input (i_e)

$$i_i = i_e + i_{fb}$$

$$A_i = \frac{i_o}{i_e}$$

$$\beta_i = \frac{i_{fb}}{i_o}$$

Interms of output (i_o)

$$i_i = \frac{i_o}{A_i} + \beta_i i_o$$

$$i_i = \frac{i_o}{A_i} [1 + \beta_i A_i]$$

$$A_{if} = \frac{i_o}{i_i} = \frac{A_i}{1 + \beta_i A_i}$$

input parameters (i_e)

$$i_i = i_e + i_{fb}$$

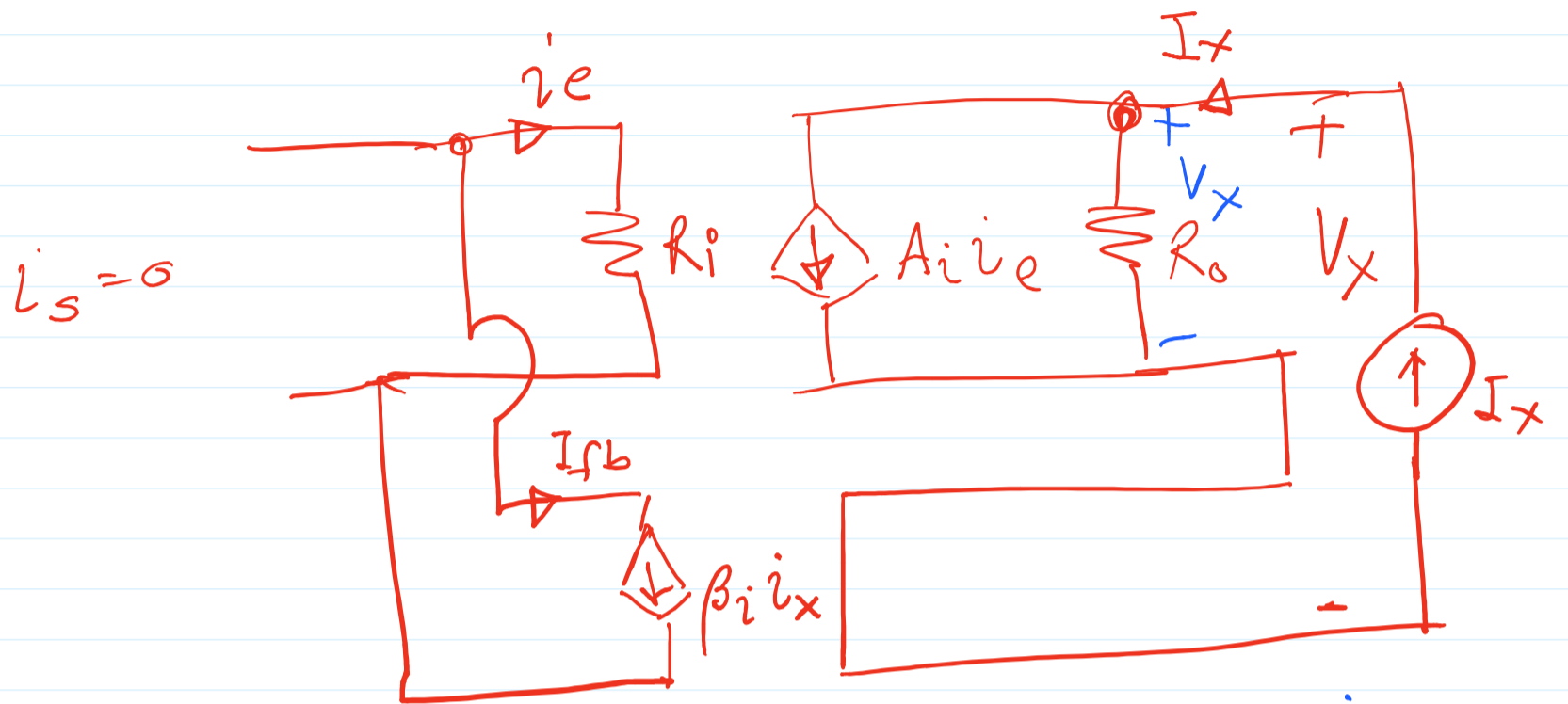
$$= i_e + \beta_i i_o$$

$$= i_e + \beta_i A_i i_e$$

$$= i_e [1 + \beta_i A_i]$$

$$R_{if} = \frac{v_i}{i_i} = \frac{v_i R_o}{i_e (1 + \beta_i A_i)}$$

$$Z_i = \frac{R_i}{1 + \beta_i A_i}$$



$$R_{of} = \frac{V_x}{I_x}$$

$$I_x = \frac{V_x}{R_o} + A_i i_e$$

$$0 = i_i = i_e + i_{fb}$$

$$i_e = -i_{fb}$$

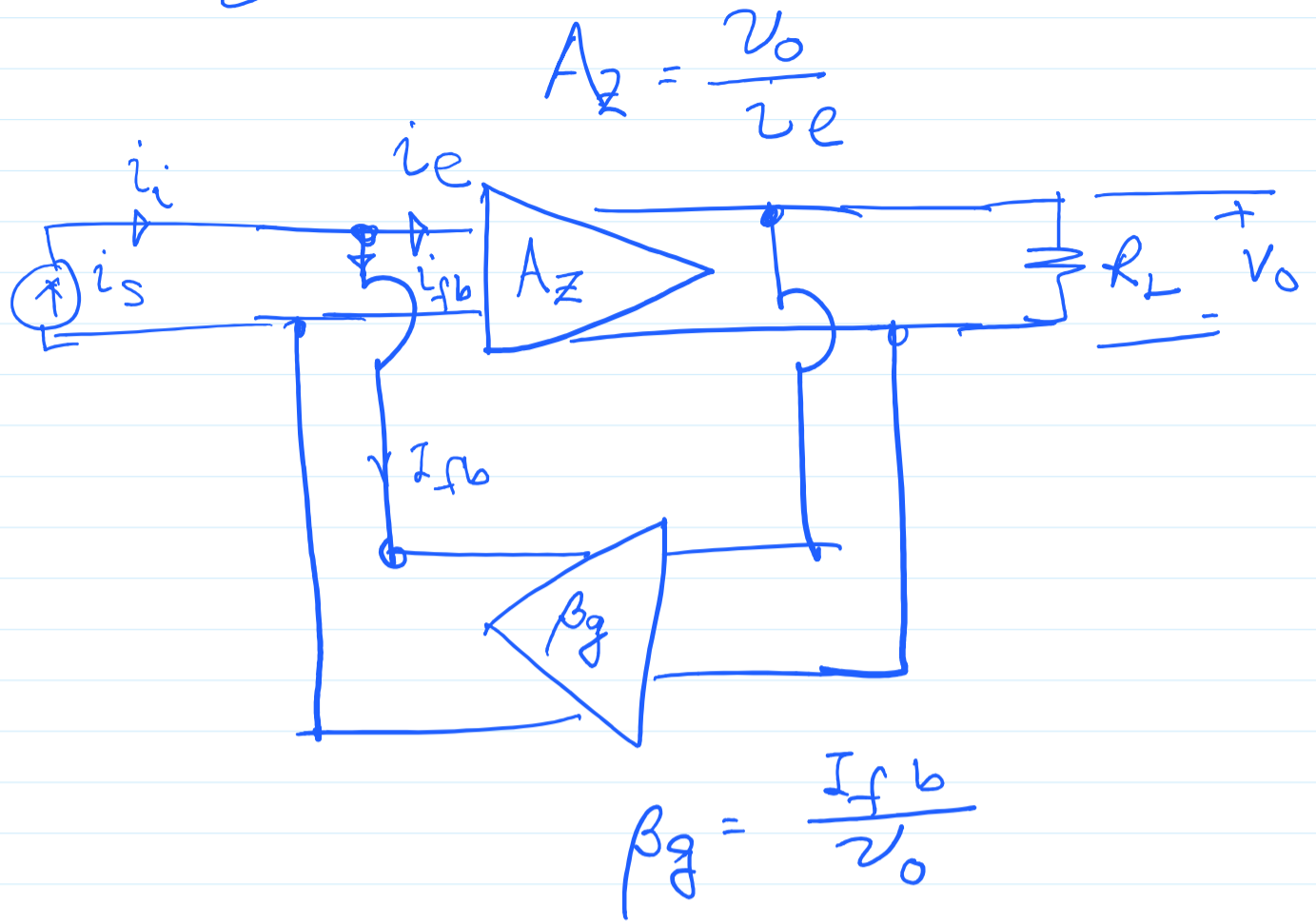
$$I_x = \frac{V_x}{R_o} - A_i i_{fb}$$

$$= \frac{V_x}{R_o} - A_i \beta_i i_x$$

$$I_x [1 + \beta_i A_i] = \frac{V_x}{R_o}$$

$$\therefore R_{of} = \frac{V_x}{I_x} = R_o [1 + \beta_i A_i]$$

shunt-shunt



Input i_e

Output v_o

$A_z = \frac{v_o}{i_e}$

$\beta_g = \frac{i_{fb}}{v_o}$

$i_i = i_e + i_{fb}$

$A_{zf} = \frac{v_o}{i_i}$

$R_{if} = ?$

$R_{of} = ?$

$i_i = i_e + i_{fb}$

$= i_e + \beta_g v_o$

$= i_e + \beta_g A_z i_e$

$= i_e [1 + \beta_g A_z]$

$\therefore R_{if} = \frac{v_i}{i_e} = \frac{v_i}{i_e (1 + \beta_g A_z)}$

A_{zf}

$i_i = \frac{v_o}{A_z} + \beta_g v_o$

$= \frac{v_o}{A_z} [1 + \beta_g A_z]$

$\therefore A_{zf} = \frac{v_o}{i_i} = \frac{A_z}{1 + \beta_g A_z}$

$= \frac{R_i}{(1 + \beta_g A_z)}$